

## HIGHLY INSULATED INDUCTIVE DATA COUPLERS

### CROSS-REFERENCE TO RELATED APPLICATIONS

5           The present application is claiming priority of U.S. Provisional Patent Application Serial No. 60/419,174, filed on October 17, 2002, the content of which is herein incorporated by reference.

### BACKGROUND OF THE INVENTION

10

#### 1. Field of the Invention

          The present invention relates to power line communications, and more particularly, to a data coupler being insulated in a manner that minimizes voltage  
15 breakdowns.

#### 2. Description of the Related Art

          An inductive coupler for power line communications couples a data signal  
20 between the power line and a communication device such as a modem. The inductive coupler may suffer from insulation breakdown or partial discharge at unsuitably low line voltages. Breakdown or partial discharge will generally occur at a location within the coupler where an electric field is concentrated in an insulating material or where an excessively high field is created through the air.

25

          FIG. 1 shows a cross-section of a prior art inductive coupler. A power line 800, e.g., a phase line, serves as a primary winding for the inductive coupler, and thus passes through an aperture of a magnetic circuit with a core configured with an upper core portion that includes a core section 805 and a lower core portion  
30 that includes a core section 810, and air gaps 830 and 835. A secondary winding 820 also passes through the aperture, surrounded by an insulating material 825.

Power line 800 touches core section 805 at a contact point 855, while secondary winding 820 is grounded. Core sections 805 and 810 are made of a magnetic core material. An electric field inside of core sections 805 and 810 depends on conductivity and permittivity of the core material.

5

For the case of power line 800 being bare, the full phase voltage is applied to the coupler, specifically between contact point 855 and secondary winding 820.

Referring to FIG. 2, for the case of power line 800 being covered with insulation, there is shown power line 800 having insulation 860 that contacts core section 805 at a contact point 865. A capacitive voltage divider is formed between (a) a capacitor formed between power line 800, insulation 860, and core section 805, and (b) a capacitance between contact point 865 and secondary winding 820. The voltage stress between contact point 865 and ground is then less than the full phase voltage.

15

A plane where secondary winding 820 exits core section 810, core section 810 presents a sharp corner. In general, there may be two locations susceptible to ionization and voltage breakdown, (1) an air path 840 between power line 800 and insulating material 825, and (2) a region between of the corners of core section 810 and the exiting of secondary winding 820 from core section 810.

20

Air path 840 is susceptible to ionization and voltage breakdown, as follows. Insulating material 825 is likely to be constructed from a plastic or other material with a permittivity of 2.5 – 3.5. A capacitive voltage division of a voltage difference between power line 800 and secondary winding 820 will place most of the voltage difference in air path 840, and relatively little of the voltage difference across an insulation path 850. The insulating capability of air is inferior to that of plastic or other insulating material, so as voltage on power line 800 increases, a breakdown is most likely across path 840.

25

30

FIG. 3 shows a horizontal cross section drawn through a secondary winding 820 such as that shown in FIG. 1. The lower core portion is shown as being configured with a plurality of core sections, namely core sections 810, 811, 812 and 813. Secondary winding 820 passes through core sections 810, 811, 812 and 813. Regions 1000, 1005, 1010 and 1015 represent regions of electric field concentration, and might cause initial insulation breakdown at a voltage on power line 800 that is much lower than desired.

#### SUMMARY OF THE INVENTION

10

The present invention relates to a data coupler being insulated in a manner that minimizes voltage breakdowns. An embodiment of the present invention is an inductive coupler for coupling a signal to a power line. The inductive coupler includes a magnetic core for placement about the power line, a coil wound around a portion of the magnetic core, and a semiconducting coating that encapsulates the core and contacts the power line. The signal is coupled to the coil.

15

Another embodiment of an inductive coupler for coupling a signal to a power line includes a magnetic core for placement about the power line, and a coil wound around a portion of the magnetic core. The coil includes a coaxial cable having an outer conductor at power line potential, and the cable includes an end with a stress cone.

20

#### BRIEF DESCRIPTION OF THE DRAWINGS

25

FIG. 1 shows a cross-section of a prior art inductive coupler, perpendicular to a power line.

FIG. 2 shows a cross-section of another embodiment of a prior art inductive coupler.

30

FIG. 3 shows a horizontal cross section drawn through secondary winding of an inductive coupler such as that of FIG. 1.

FIG. 4 is a cross section of a highly insulated inductive data coupler,  
5 perpendicular to a power line.

FIG. 5 shows a horizontal cross section drawn through a lower core portion of a highly insulated inductive data coupler, such as that of FIG. 4.

10 FIG. 6 is a vertical cross-section through an arrangement employing an inductive coupler having a semiconductive coating.

FIG. 7 is a cross section of a high voltage inductive data coupler that incorporates a cable as a secondary winding.

15

#### DESCRIPTION OF THE INVENTION

A highly insulated inductive data coupler, in accordance with the present invention, virtually eliminates high electric fields through air paths, and limits  
20 those fields to locations filled with dielectric material. Rounded geometries are employed on all energized bodies to eliminate any pointy features that might generate a high local field. Also, upper and lower core portions are placed inside a single common equipotential envelope, making the coupler indifferent to dielectric properties of magnetic cores, and eliminates electric fields within the  
25 cores and between upper and lower core portions.

FIG. 4 is a cross section of a highly insulated inductive data coupler in accordance with the present invention. The coupler includes a magnetic core for placement about power line 800. The magnetic core is configured with an upper  
30 core portion that includes core section 805 and a lower portion that includes core section 810. The designation of core portions as being "upper" and "lower"

merely refers to their respective positions in the drawings of the present disclosure, and such designation is not necessarily descriptive of an actual physical relationship of the core portions. Secondary winding 820 is connected to a communication device (not shown) such as a modem, and thus, the coupler  
5 enables a data signal to be coupled between power line 800 and the communication device.

Each of core section 805 and core section 810 are encapsulated in boots or coatings 900 and 905 made of a semiconductor material. Examples of suitable  
10 semiconductor materials are plastics or rubbers impregnated with graphite or silicon carbide to provide a desired bulk resistivity. An electrical contact 910 is made between coating 900 and coating 905. Core sections 805 and 810 and coatings 900 and 905 thus become a single, essentially equipotential body.

15 A surface 915 of insulating material 825 is covered with a semiconducting coating 945, which overlaps coating 905 and makes electrical contact with coating 905. The potential of coating 945 is thus made essentially equal to the surface of power line 800, eliminating or greatly reducing the voltage across an air path 940. This permits an inductive coupler that includes secondary winding 820 and core  
20 sections 805 and 810, and employs power line 800 as a primary winding, to be safely used on higher primary voltages than would be possible without semiconducting coating 945.

FIG. 5 shows a horizontal cross section drawn through a lower core portion  
25 of a highly insulated inductive data coupler, such as that of FIG. 4. The lower core portion is, in turn, configured with a plurality of core sections, namely core sections 810, 811, 812 and 813. The inductive data coupler of FIG. 5, when compared to that of FIG. 3, experiences a reduction of field concentration in region 1105, as compared to region 1000, at the exit of the secondary winding 820  
30 from core section 813. Coating 905 is equipped with a rounded profile 1100, which provides a rounded extension to the side of core section 813. Rounding the

shapes of energized bodies, such as core section 813, reduces the maximum electric field in region 1105 for a given voltage carried on power line 800 (FIG. 1). Conversely, for a given insulating material 825 (FIG. 1) having a maximum voltage breakdown rating, the applied voltage on power line 800 may be

5 increased, relative to that permissible when sharp corners are present.

Secondary winding 820 is shown in FIG. 5 with a single pass through the core. In practice, secondary winding 820 may be configured as a coil, wound around a portion of the core.

10

There is thus provided an inductive coupler for coupling a signal to a power line. The inductive coupler includes (a) a magnetic core for placement about the power line, (b) a coil wound around a portion of the magnetic core, where the signal is coupled to the coil, and (c) a semiconducting coating that encapsulates

15 the core and contacts the power line. The core has a longitudinal end, and so the inductive coupler also includes a rounded semiconducting body that covers the longitudinal end and is in electrical contact with the semiconducting coating. The coil has a lead emerging from the core, and so the inductive coupler also includes a semiconducting layer over the end, to reduce electrical stress between the power

20 line and a surface of an insulation covering the coil.

FIG. 6 is a vertical cross-section through an arrangement employing an inductive coupler having a semiconductive coating. An air path 1200 is susceptible to ionization and breakdown between power line 800 and a surface

25 1210 of an insulating layer 1225 surrounding a grounded secondary winding 1220. A potential difference between power line 800 and secondary winding 1220 is capacitively divided between air path 1200 and insulating layer 1225. A greater proportion of the potential difference occurs across air path 1200 as compared to the potential difference across insulating layer 1225, and air path 1200 is also the

30 poorer insulator.

To mitigate this situation, a technique similar to that used in stress cones is employed. A stress cone is used at the termination of two conductor cables and provides a gradual decrease of electric potential so as to reduce field concentrations that might lead to insulation breakdown. This is illustrated on the right half of FIG. 6. Embedded in insulating layer 1225, a semiconducting layer 1230 is sandwiched between secondary winding 1220 and a surface 1215 of insulating layer 1225, and connected to coating 905 of core sections 805 and 810. Semiconducting layer 1230 includes a combination of series resistance and stray capacitance that causes potential to decrease with distance from the longitudinal end of the semiconductive core coating 905, avoiding any excessive electrical stress concentration at the distal edge of semiconducting layer 1230. Semiconducting layer 1230 thus raises the potential of surface 1215 to be close to the primary potential of power line 800, greatly reducing the potential difference across air path 1205, and preventing breakdown at unacceptably low primary voltages on power line 800.

Secondary winding 1220 is shown in FIG. 6 with a single pass through the core. In practice, secondary winding 1220 may be configured as a coil, wound around a portion of the core.

Eliminating large potential differences across air paths and eliminating points of high electrical stress can be achieved by a combination of techniques. In one technique, the cores are coated by a semiconducting layer, as described above in association with FIGS 4 and 5. For another technique, a section of high voltage cable is employed or specially molded for the coupler. The cable has an external semiconducting layer that is energized by conductive or capacitive contact with coated magnetic cores. The cable has a center conductor that is grounded. At the two ends of a secondary winding, stress cones provide a termination of the cable. Indoor stress cones without sheds may be used if the secondary is embedded in insulation. Otherwise, outdoor stress cones with sheds to increase the leakage path may be used.

FIG. 7 is a cross section of another embodiment of a high voltage inductive data coupler 1345, in accordance with the present invention. Coupler 1345 uses a high voltage cable as a secondary winding.

5

Power line 800 passes through core section 805, which is coated by a semiconducting layer 900. A secondary winding 1300, i.e., an inner conductor of a secondary cable 1305, is grounded via chokes (not shown), and passes through a core section 810, which is encapsulated in a semiconducting layer 905. Secondary cable 1305 is coated with a semiconducting layer 1310, which connects to a semiconducting portion 1315 of a stress cone 1320. The entire lower portion of coupler 1345 is encapsulated in an insulating body 1325, equipped with sheds 1330 to provide a long leakage path between power line 800 and grounded secondary winding 1300.

15

Functionally, power line 800, or its thin insulation, contacts semiconducting layer 900 and brings the potential of semiconductor layer 900 close to the potential of power line 800. The terms “gap” and “air gap” are used to indicate a non-magnetic spacer or non-magnetic region between parts of a core, to increase current handling capacity and maximum magnetomotive force before saturation. Semiconducting layer 900 contacts semiconducting layer 905 at a gap 1350 between core sections 805 and 810, respectively, bringing semiconducting layer 905 close to the potential of power line 800. Secondary cable 1305 has its semiconducting layer 1310 in direct contact with semiconducting layer 905, thus also bringing semiconducting layer 1310 to a potential close to that of power line 800.

At each end of secondary cable 1305, a stress cone 1320 terminates secondary cable 1305, allowing secondary winding 1300 to exit coupler 1345 without undue local electrical stress. An air path 1340 does not bridge a high

30



potential, as the potential of the surface of coupler 1345 is near the potential of power line 800 due to the underlying energized semiconducting layer 1310.

5       Secondary cable 1305 is shown in FIG. 7 with a single pass through the core. In practice, secondary cable 1305 may be configured as a coil, wound around a portion of the core.

10       There is thus provided another embodiment of an inductive coupler for coupling a signal to a power line. The inductive coupler includes (a) a magnetic core for placement about the power line, (b) a coil wound around a portion of the magnetic core, where the signal is coupled to the coil, and (c) a semiconducting coating that encapsulates the core and contacts the power line. Furthermore, the coil has a section of high voltage cable coated with semiconducting material, the semiconducting material being in conductive or capacitive contact with  
15       semiconducting coating, and inductive coupler also includes a stress cone at an end of the coil.

20       It should be understood that various alternatives, combinations and modifications of the teachings described herein could be devised by those skilled in the art. The present invention is intended to embrace all such alternatives, modifications and variances that fall within the scope of the appended claims.